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## Frequency Domain Modelling of a Compressible Wave Energy Device

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### ABSTRACT

The present study focuses on numerical modelling of the SQ1 device, a floating wave energy converter comprised of two volumes (see Fig. 1): an air bag, constructed of fabric and an array of tendons, and a rigid volume housed within the device. As the device heaves in waves, the bag expands and contracts leading to air being exchanged between the volumes, driving a turbine located in between the two. Due to the compressibility of the volume, the SQ1 device can have a heave resonance period longer than that of a rigid body of equivalent mean geometry, potentially reducing the size and cost of the device. The aim of the present work is to compare the device response, power production and structural loads of the SQ1 device, with that of a rigid body of the same mean geometry.

A linear frequency domain model has been developed based on the assumptions that the SQ1 device is axisymmetric, the tension in the fabric is zero, and that all of the tension is carried by the tendons. This simplifies the focus of the numerical model to a single tendon. The tendon is initially considered as inextensible, but the model will be adapted to incorporate linear elastic properties, allowing different materials to be evaluated. The shape of the tendon at the equilibrium position of the device is calculated first [2], and is unique for a specified internal pressure in the bag, ballast, and the submergence of the bottom of the bag. In waves of small amplitude, the device is assumed to oscillate around this mean tendon geometry, and is dependent on hydrodynamic coefficients calculated through the generalized mode functionality of the wave-structure interaction analysis software WAMIT [3]. Preliminary results from the numerical model show good agreement with small scale experimental data obtained in the 35m x 15.5m wave basin at the COAST laboratory, Plymouth University [1]. Full scale results based on a representative installation site will also be presented.

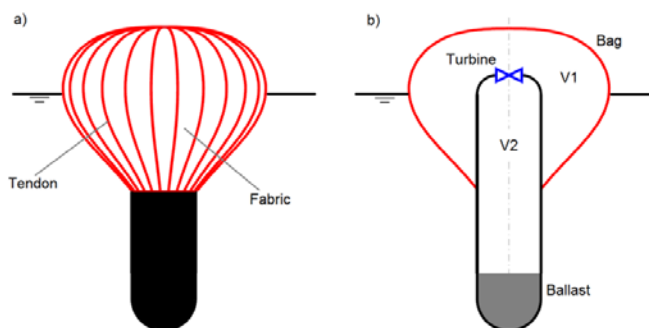


Figure 1: Sketch of the SQ1 device showing a) the fabric and tendon construction of the bag, and b) a cross-section of the device with the main components labelled.

### REFERENCES

- [1] A. Kurniawan, J. Chaplin, D. Greaves and M. Hann, "Wave energy absorption by a floating air bag," *J. Fluid Mech.*, vol. 812, pp. 294-320, 2017.
- [2] J. Chaplin, F. Farley, D. Greaves, M. Hann, A. Kurniawan, M. Cox, "Numerical and experimental investigation of wave energy devices with inflated bags", In *Proceedings of 11<sup>th</sup> European Wave and Tidal Energy Conference, Nantes, France, 2015*
- [3] WAMIT, "WAMIT User Manual V. 7.1", Chestnut Hill, MA, [www.wamit.com](http://www.wamit.com), 2017